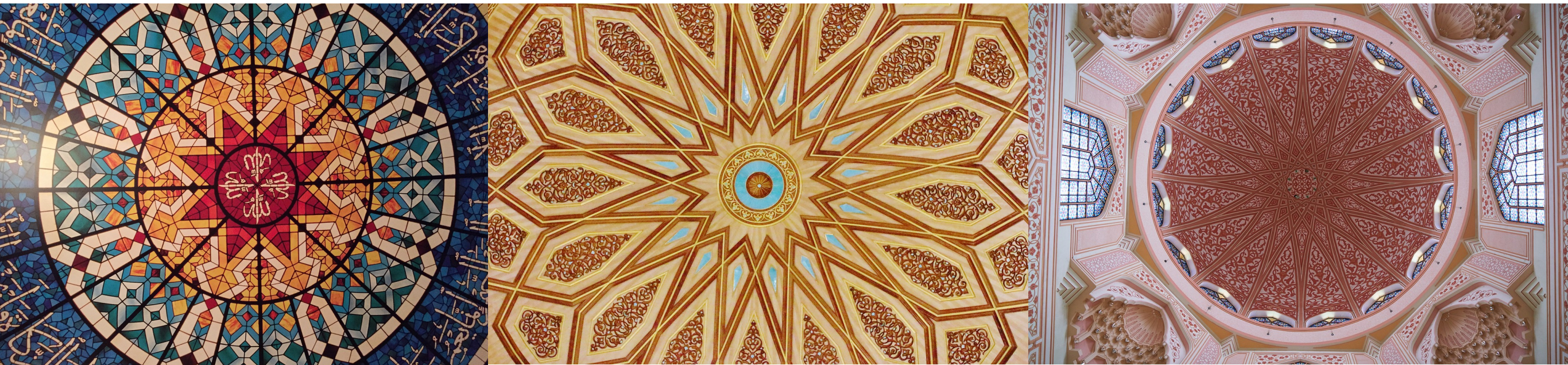




MECHANICAL VIBRATION

BMCG 3233

CHAPTER 4: HARMONIC FORCED VIBRATION (PART 1)

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4.1 Undamped Forced Vibration

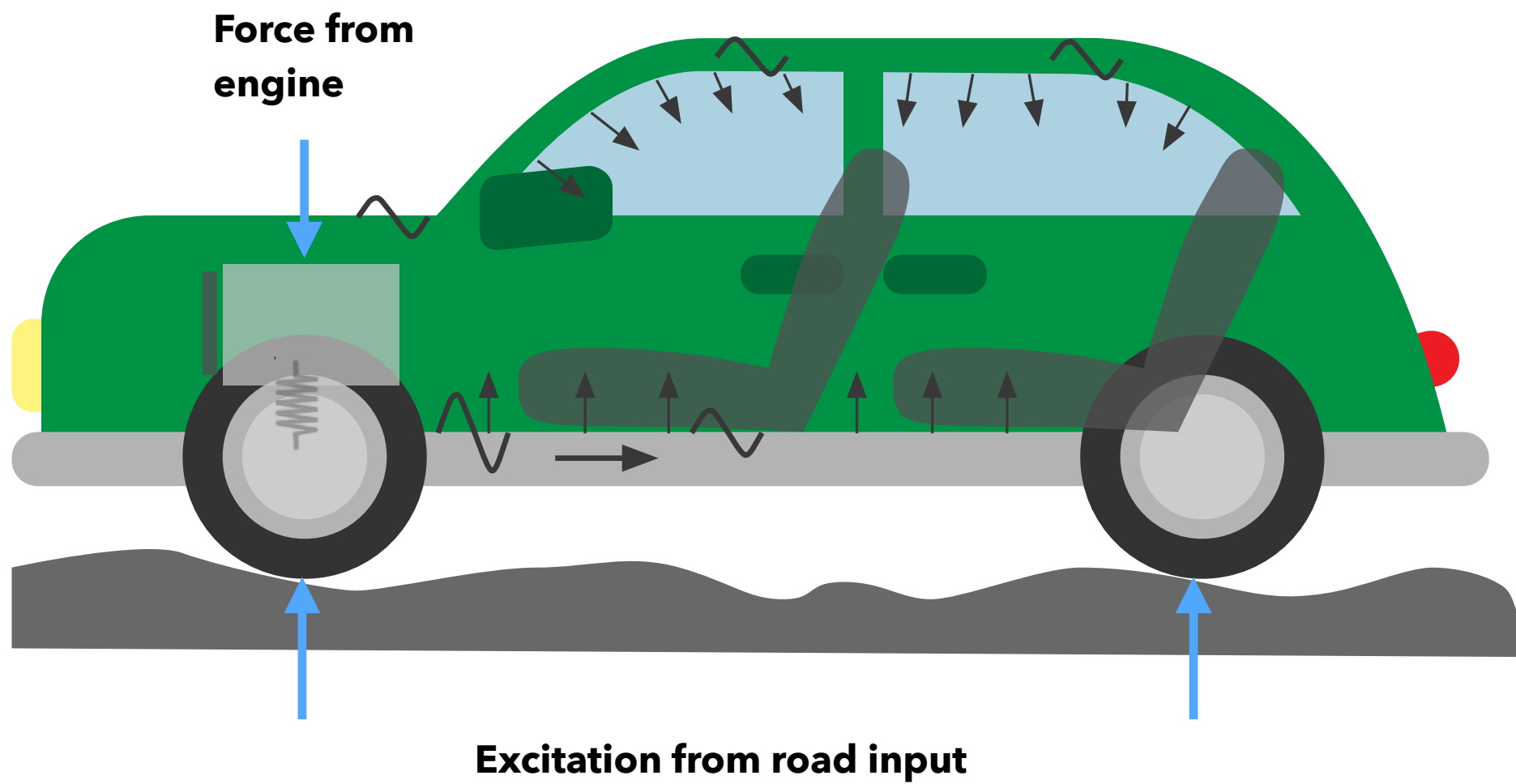
4.2 Damped Forced Vibration

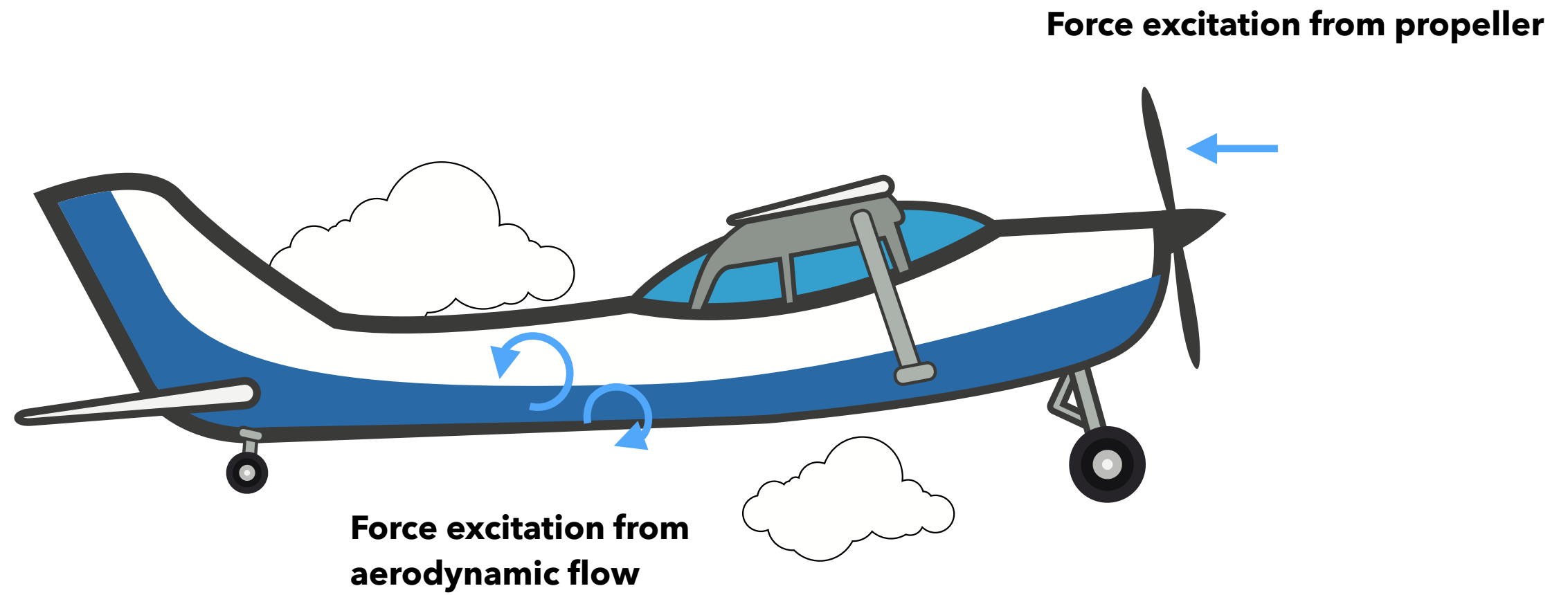
LEARNING OBJECTIVES

1. Derive the Frequency Response Function
2. Solve vibration problem due to damped forced vibration.

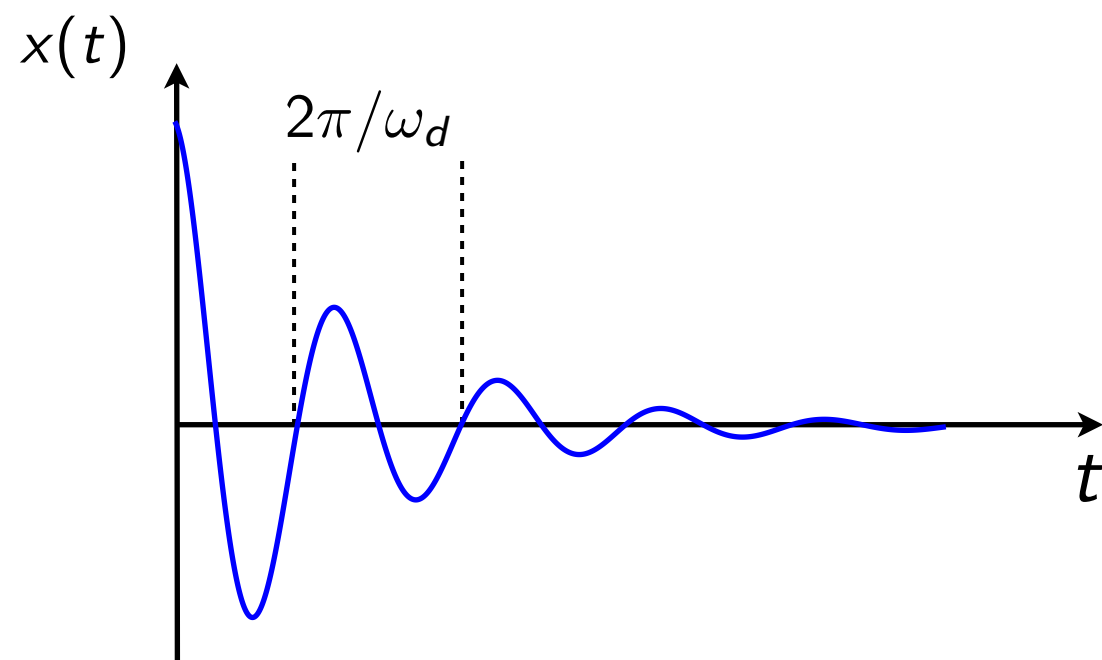


Vibration caused by **force** exciting the structure



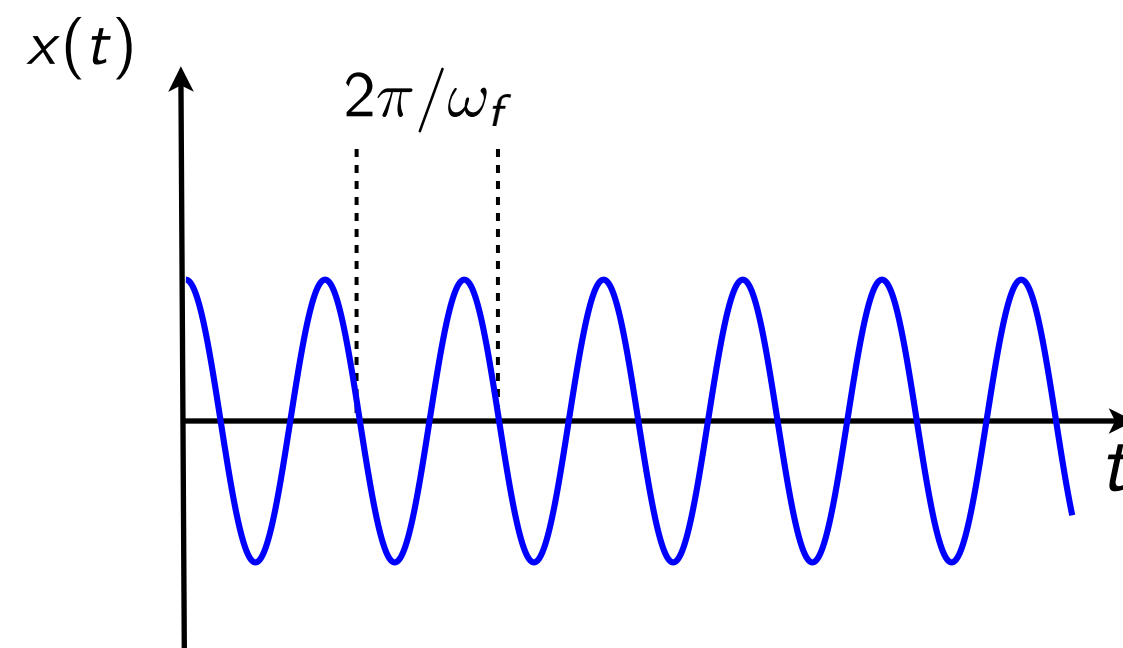


Free vibration



Vibration decays to zero

Forced vibration

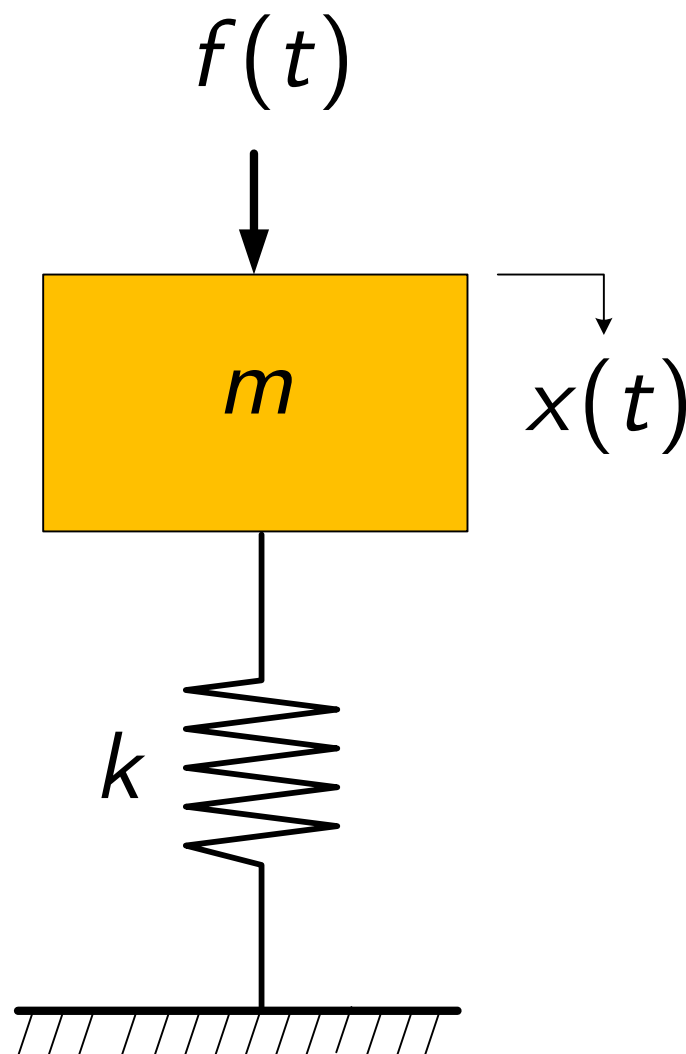


**Vibration keeps going forever,
as long as the force still exists**



4.1

UNDAMPED FORCED VIBRATION



Equation of motion:

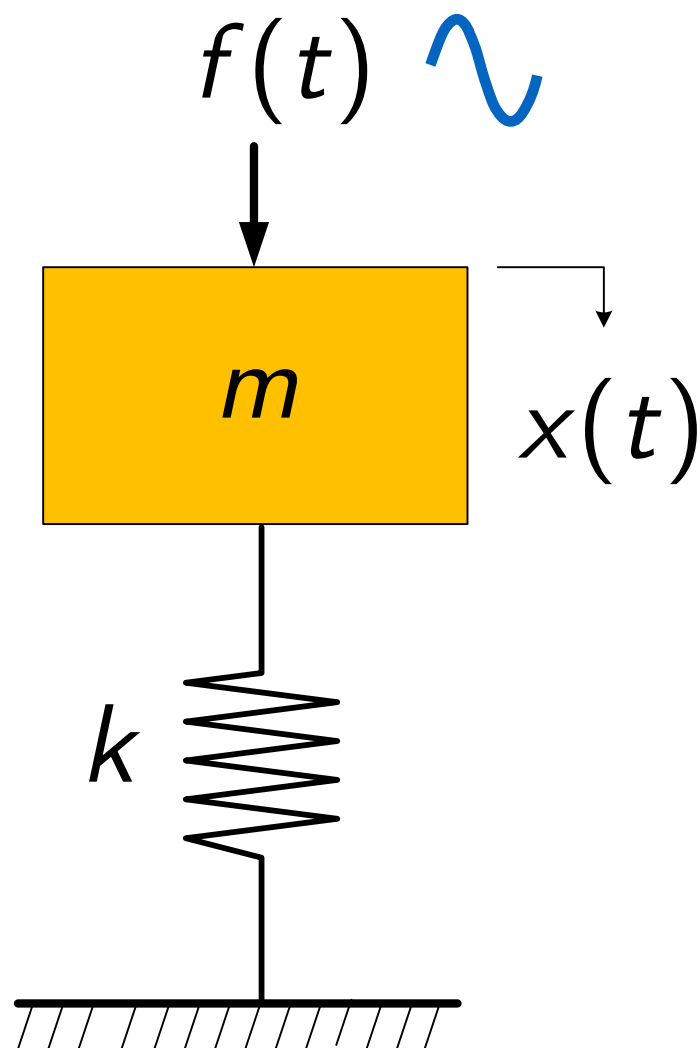
$$m\ddot{x}(t) + kx(t) = f(t)$$

Force $f(t)$ can be:

- **Time harmonic** - rotating machine
- **Transient** (finite duration) - bump or impact
- **Random** (unpredictable) - wind load

We will focus on time **harmonic** excitation:

$$f(t) = F \sin(\omega t + \phi)$$



For harmonic force, equation of motion:

$$m\ddot{x}(t) + kx(t) = F \sin(\omega t + \phi)$$

Response will also be harmonic:

$$x(t) = X \sin(\omega t + \phi)$$

Magnitude of $x(t)$

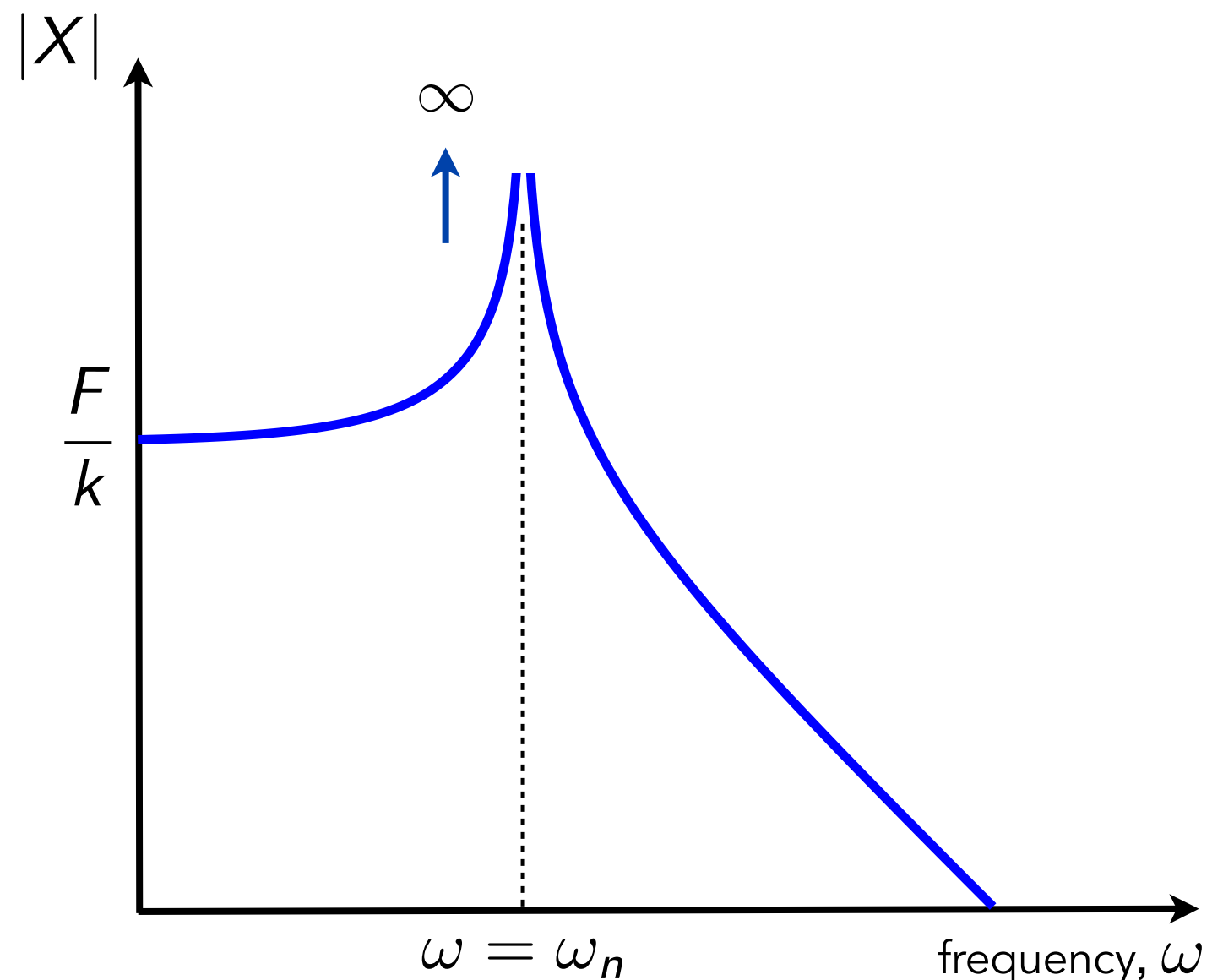
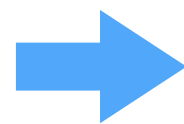
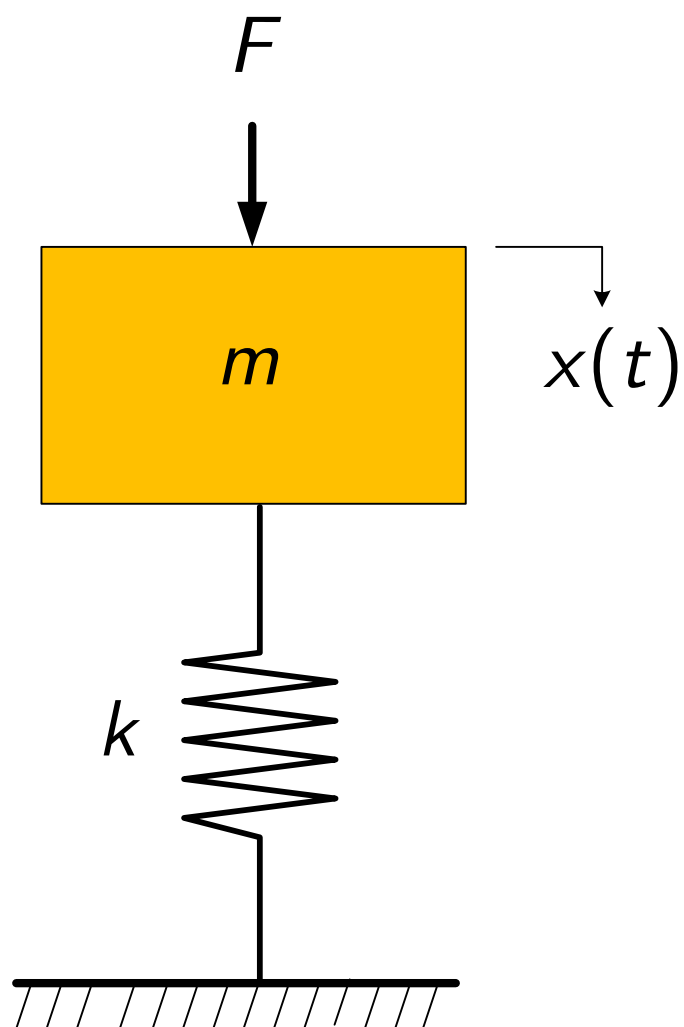
This gives steady-state vibration amplitude:

$$X = \frac{F}{k - \omega^2 m}$$

$$X = \frac{F}{k - \omega^2 m} = \frac{F}{k} \left(\frac{1}{1 - (\omega/\omega_n)^2} \right)$$

Excite this system with whole **frequency** of excitation

Characteristic of the SDOF system when excited with dynamic force



Static force ($\omega = 0$):

$$X = \frac{F}{k}$$

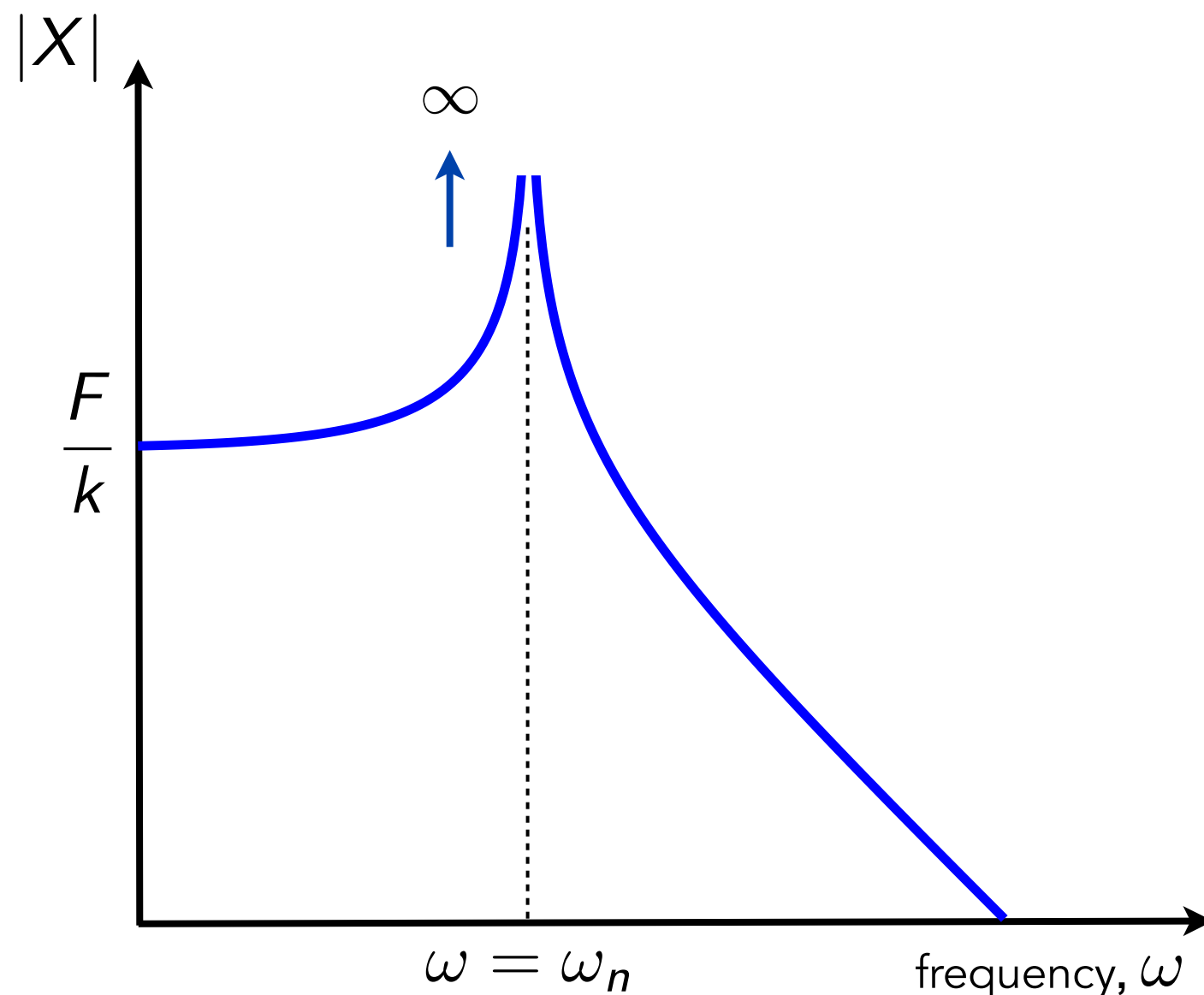
Dynamic force:

X depends on ω

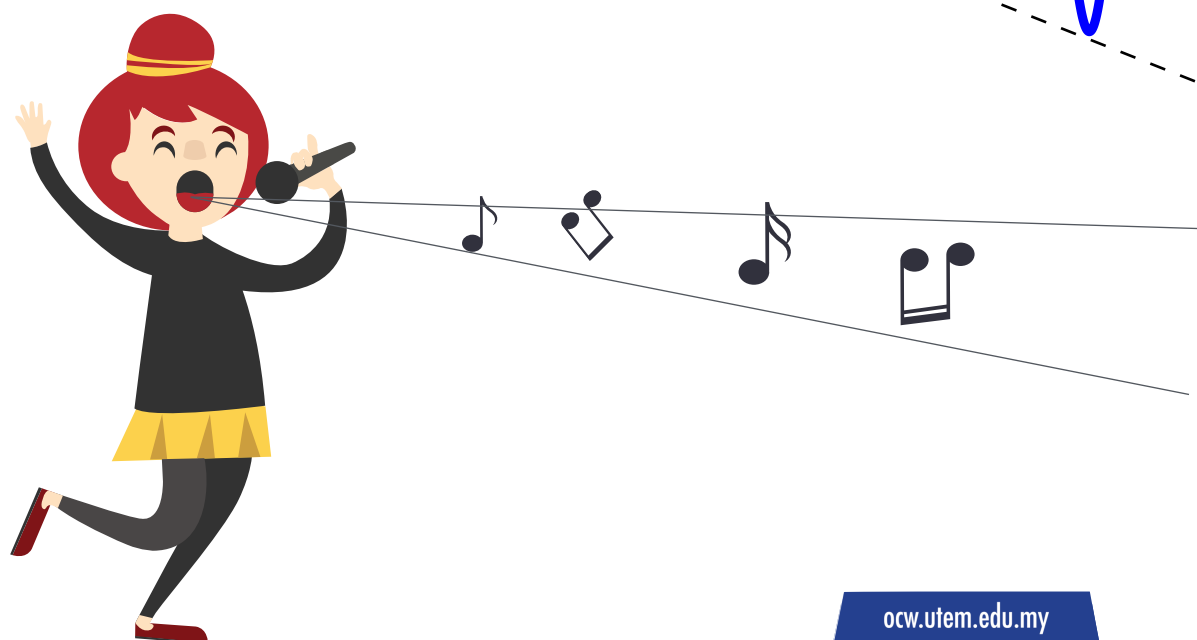
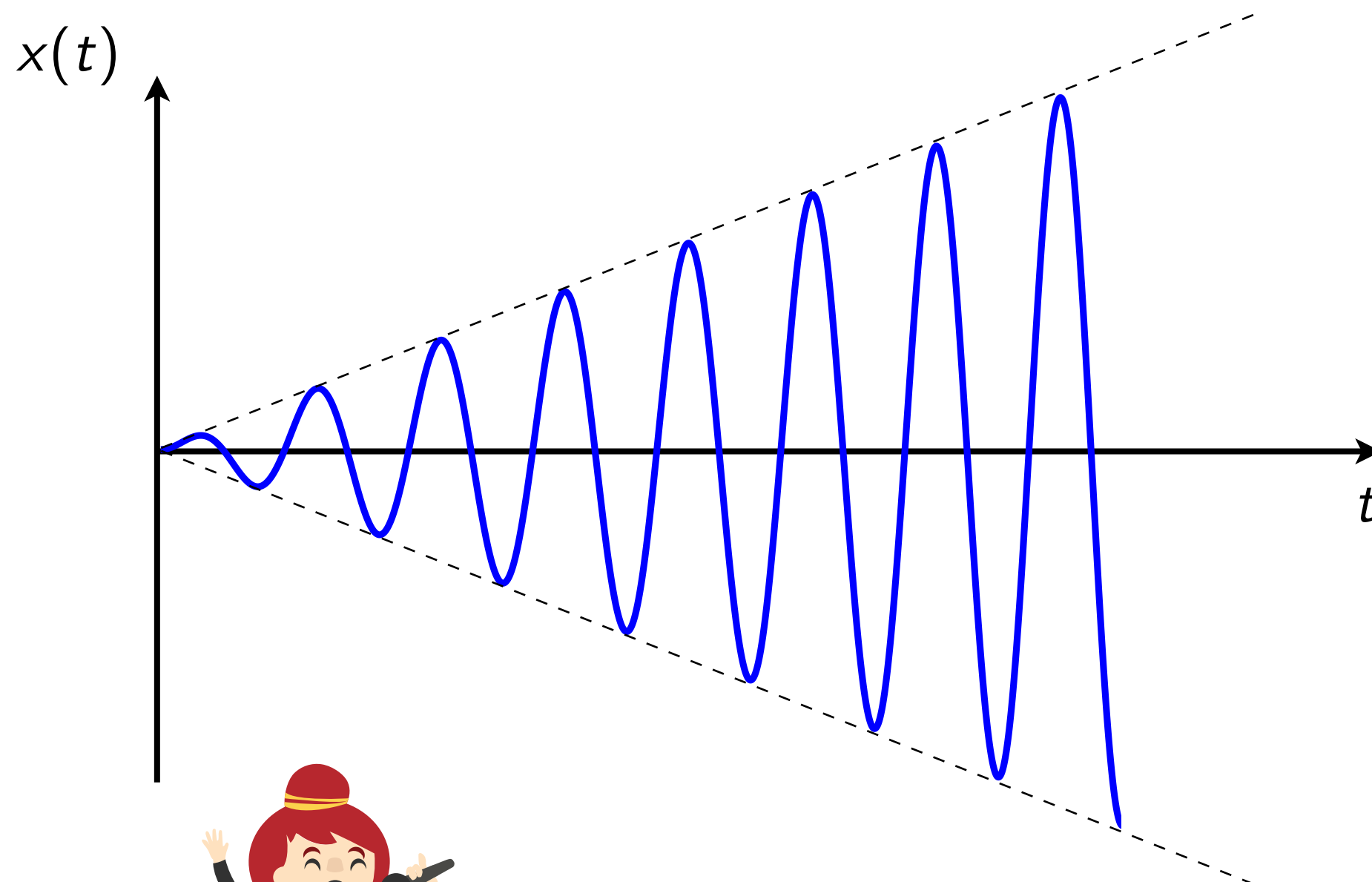
If $\omega = \omega_n$:

X becomes very LARGE!!

RESONANCE



Time response of undamped vibration at **resonance**.



**When the frequency of the voice from
a Soprano singer matches
the natural frequency of the glass.**



It happened in 1940, when resonance from the wind destroyed this massive structure - Tacoma Bridge, Washington, USA.



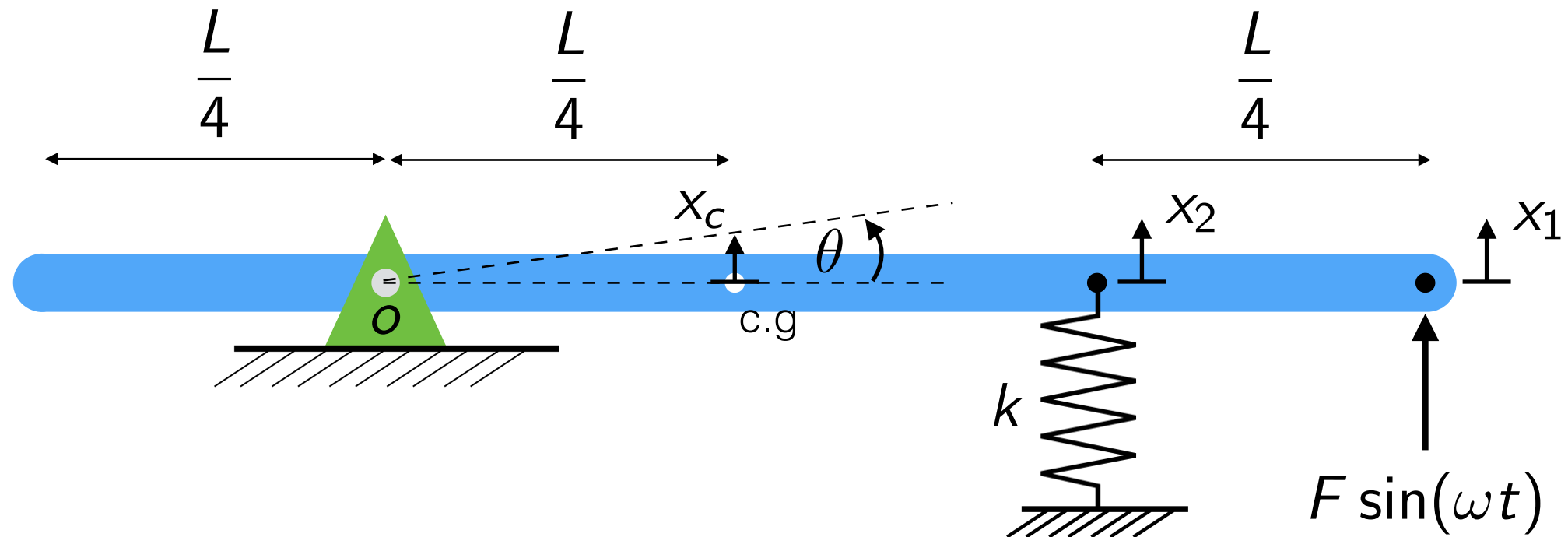


As a vibration engineer, your job is to ensure that a designed structure has **natural frequency** away from the frequency of the excitation force.

Example 4.1

Calculate the magnitude of the Frequency Response Function (FRF)!

Use x_1 as the generalised coordinate.



Use the D'Alembert principle

The external moment at point O :
$$\sum (M_{\text{ext}})_O = -kx_2 \left(\frac{L}{2} \right) + F \sin(\omega t) \left(\frac{3L}{4} \right)$$

The inertial moment at point O :
$$\sum (M_{\text{int}})_O = J\ddot{\theta} + m\ddot{x}_c \left(\frac{L}{4} \right)$$

The D'Alembert principle:

$$\sum (M_{\text{ext}})_o = \sum (M_{\text{int}})_o$$

$$-kx_2 \left(\frac{L}{2} \right) + F \sin(\omega t) \left(\frac{3L}{4} \right) = J\ddot{\theta} + m\ddot{x}_c \left(\frac{L}{4} \right)$$

Re-arrange:

$$J\ddot{\theta} + m\ddot{x}_c \left(\frac{L}{4} \right) + kx_2 \left(\frac{L}{2} \right) = F \left(\frac{3L}{4} \right) \sin(\omega t)$$

$x_2 = \frac{1}{3}x_1$
 $\ddot{x}_c = \frac{1}{3}\ddot{x}_1$
 $\ddot{\theta} = \left(\frac{4}{3L} \right) \ddot{x}_1$

After substitution:

$$\left(\frac{4J}{3L}\right) \ddot{x}_1 + \left(\frac{mL}{12}\right) \ddot{x}_1 + \left(\frac{kL}{6}\right) x_1 = F \left(\frac{3L}{4}\right) \sin(\omega t)$$

Simplified:

$$\left(\frac{16J}{L^2} + m\right) \ddot{x}_1 + 2kx_1 = 9F \sin(\omega t)$$

We are interested in steady-state response, we can use C.E. N.

The force can be expressed as $f(t) = Fe^{j\omega t}$ and substitute: $x_1(t) = X_1 e^{j\omega t}$

$$-\omega^2 \left(\frac{16J}{L^2} + m\right) X_1 + 2kX_1 = 9F \quad (*)$$

From (*), the Frequency Response Function (FRF):

$$\left| \frac{X_1}{F} \right| = \frac{9}{2k - \omega^2 \left(\frac{16J}{L^2} + m \right)}$$

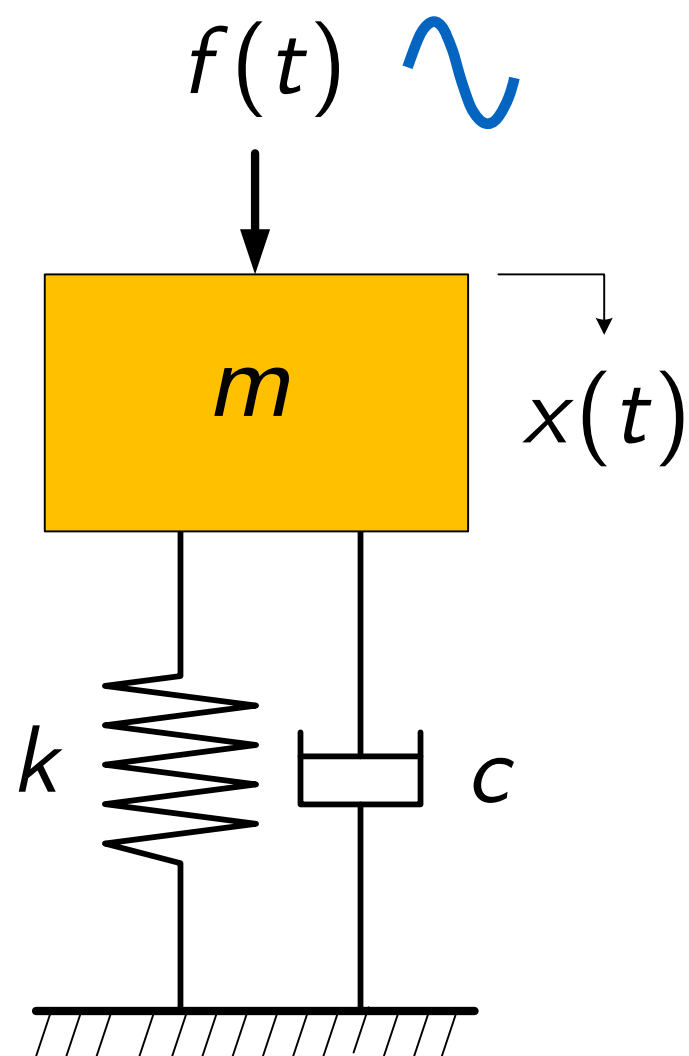
The displacement per unit force.

This FRF is called **RECEPTANCE**.



4.2

DAMPED FORCED VIBRATION

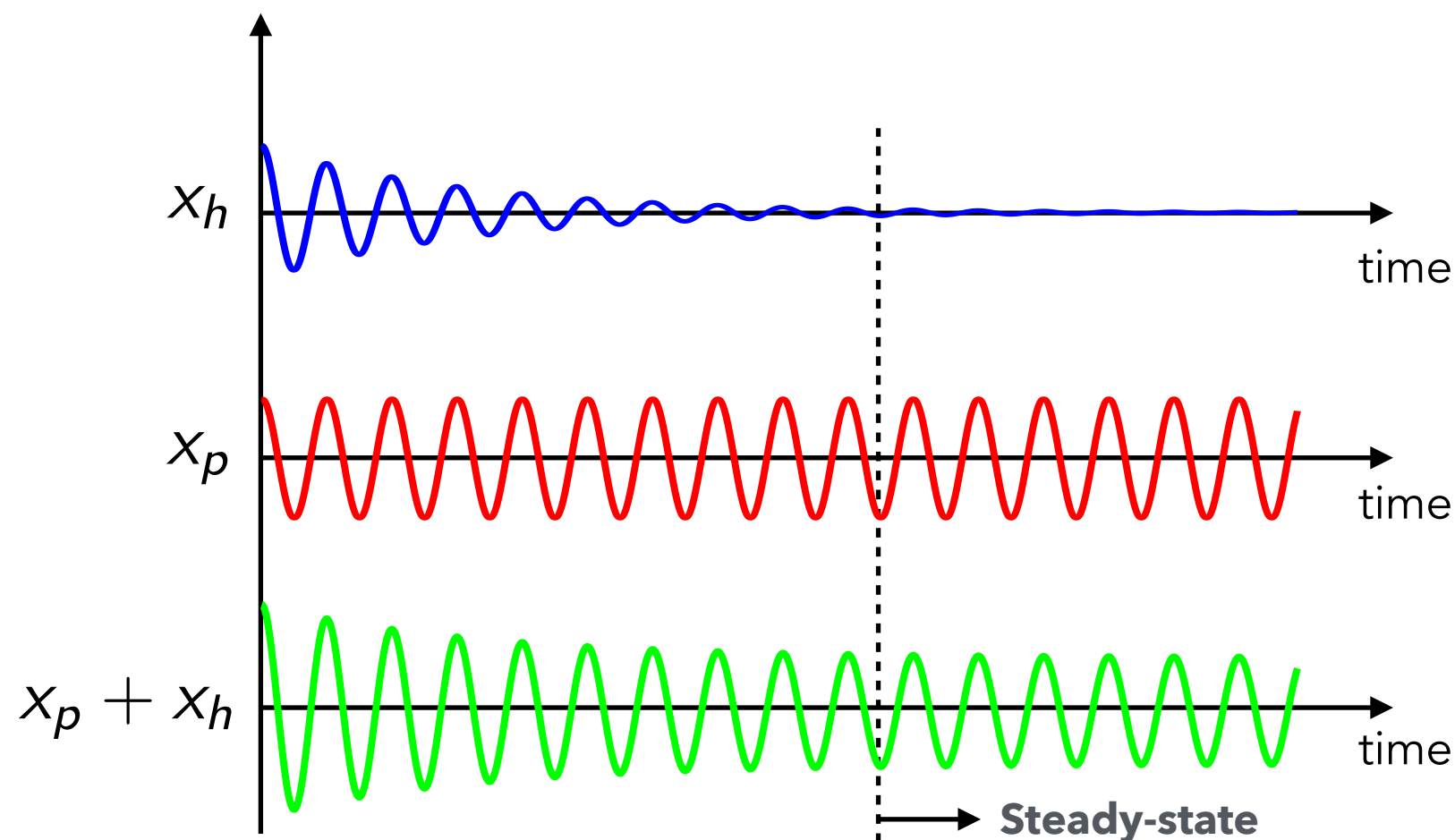


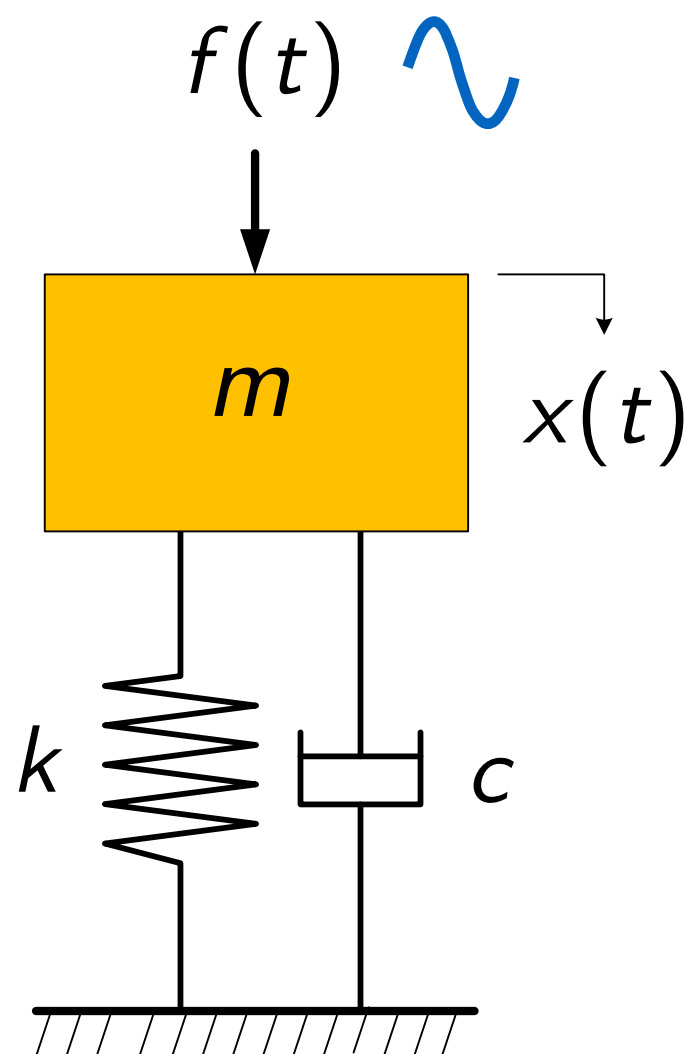
Equation of motion:

$$m\ddot{x}(t) + c\dot{x}(t) + kx(t) = f(t)$$

Homogeneous
solution, x_h

Particular
solution, x_p





Equation of motion:

$$m\ddot{x}(t) + c\dot{x}(t) + kx(t) = f(t)$$

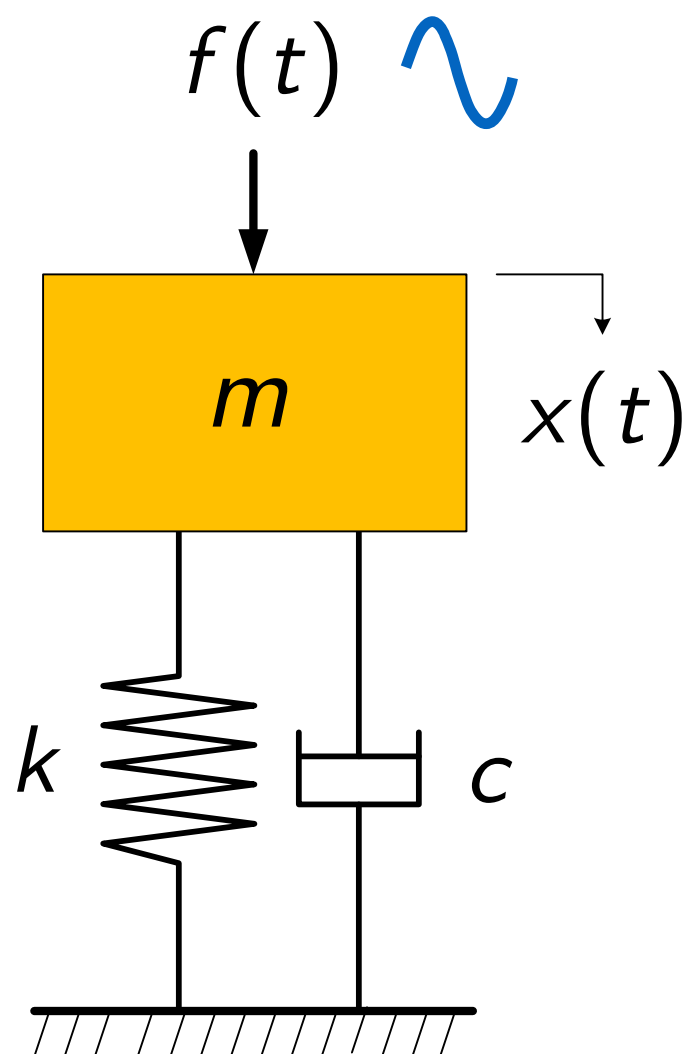
We are interested in the **steady-state response**.

For convenience, we can use the complex exponential notation:

$$f(t) = Fe^{j\omega t}, \quad x(t) = Xe^{j\omega t}$$

Complex amplitude of $f(t)$

Complex amplitude of $x(t)$



We obtain ratio of displacement to force:

$$\frac{X}{F} = \frac{1}{k - m\omega^2 + j\omega c}$$

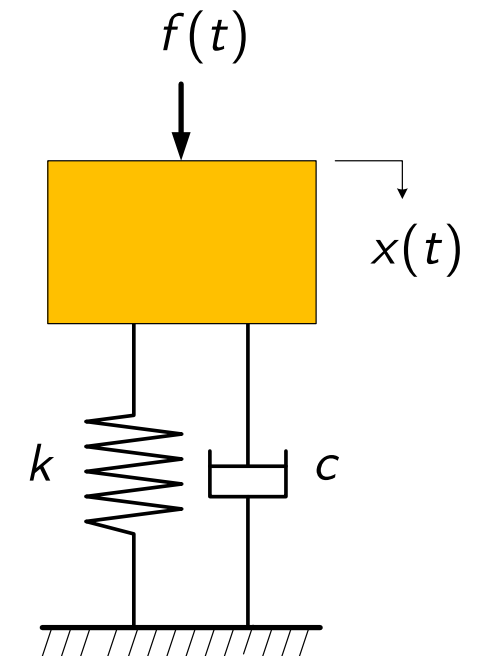
Using $\omega_n^2 = k/m$ and $c = 2\zeta\omega_n m$

We can have another expression:

$$(*) \quad \frac{X}{F} = \frac{1}{k} \left(\frac{1}{1 - (\omega/\omega_n)^2 + j2\zeta\omega/\omega_n} \right)$$

The magnitude of * as a **function of frequency**:

$$\left| \frac{X}{F} \right| = \frac{1/k}{\sqrt{\left[1 - \left(\frac{\omega}{\omega_n} \right)^2 \right]^2 + 4\zeta^2 \frac{\omega^2}{\omega_n^2}}}$$



Usually called **Frequency Response Function (FRF)**

Low frequency: $\omega \ll \omega_n \Rightarrow |X/F| = 1/k$

Stiffness controlled

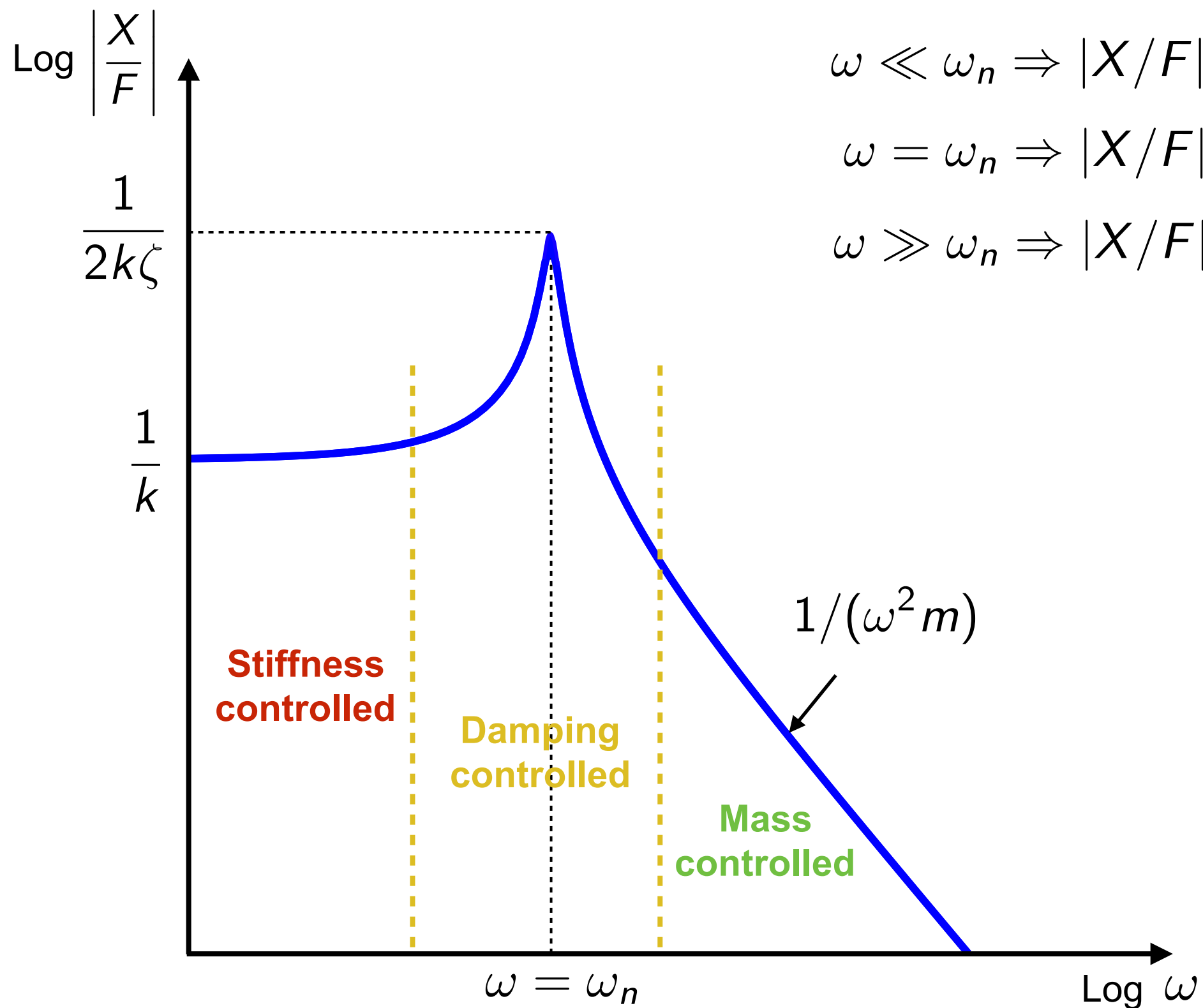
Resonance: $\omega = \omega_n \Rightarrow |X/F| = 1/(2\zeta k)$

Damping controlled

High frequency: $\omega \gg \omega_n \Rightarrow |X/F| = 1/(\omega^2 m)$

Mass controlled

FRF graph

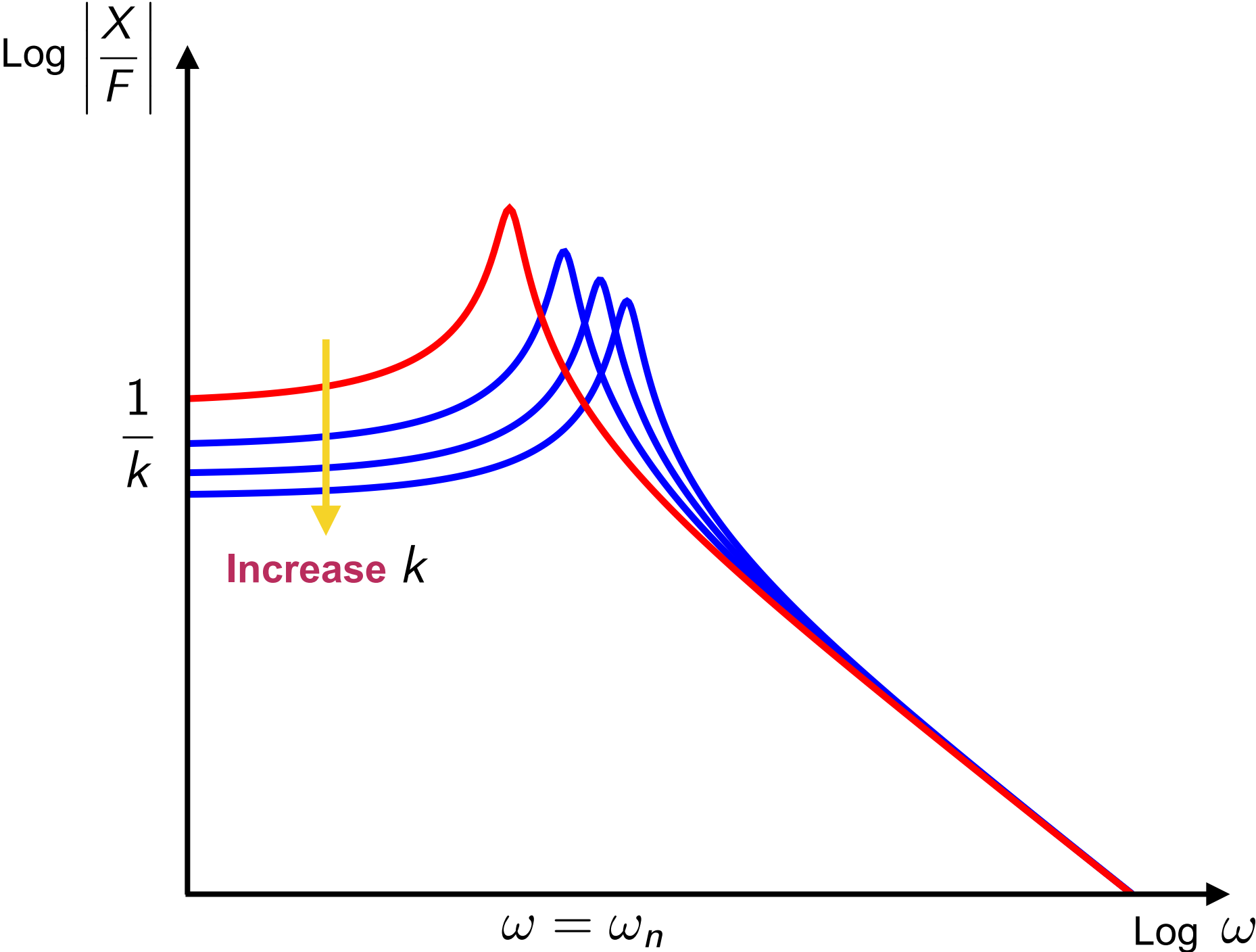


$$\omega \ll \omega_n \Rightarrow |X/F| = 1/k$$

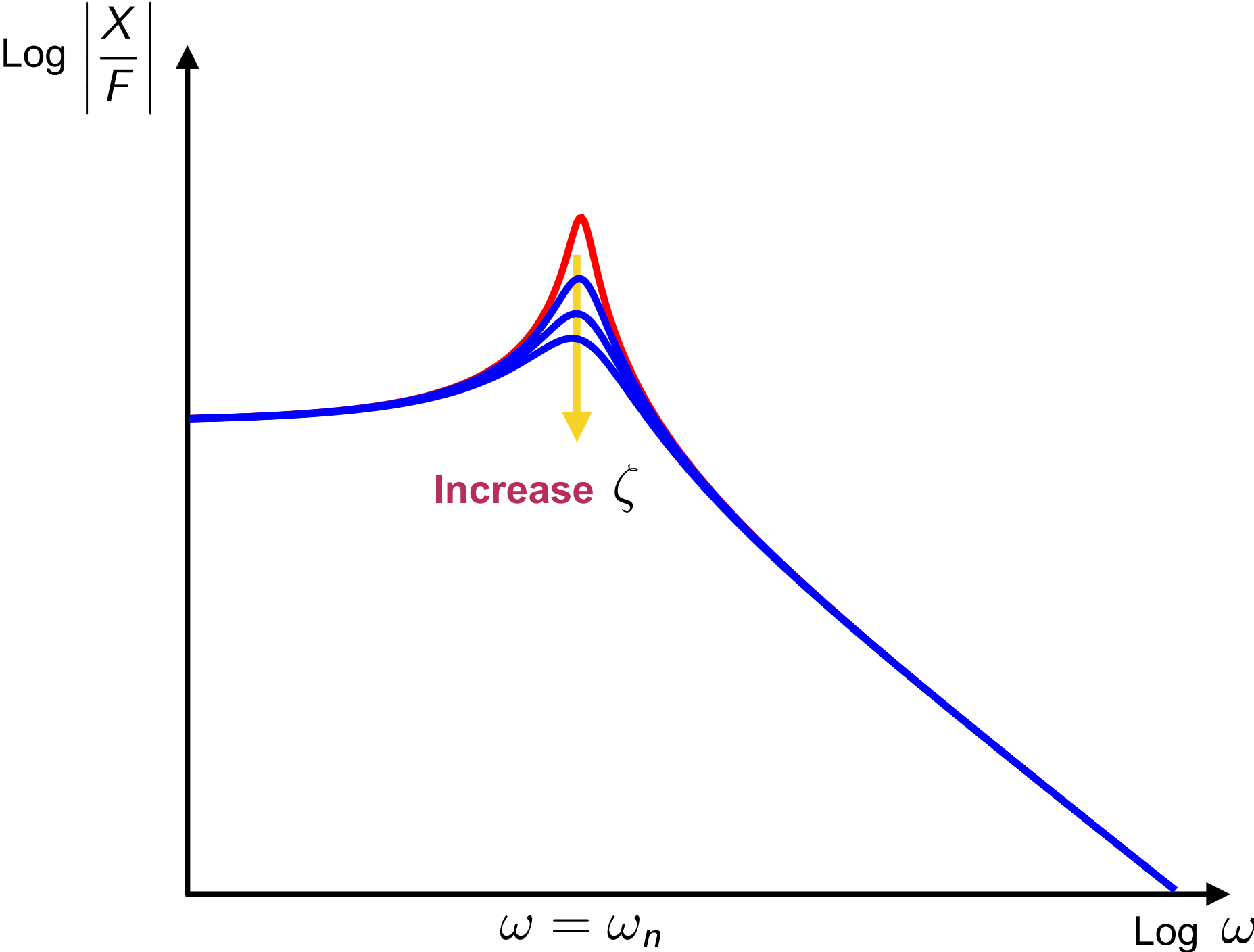
$$\omega = \omega_n \Rightarrow |X/F| = 1/(2\zeta k)$$

$$\omega \gg \omega_n \Rightarrow |X/F| = 1/(\omega^2 m)$$

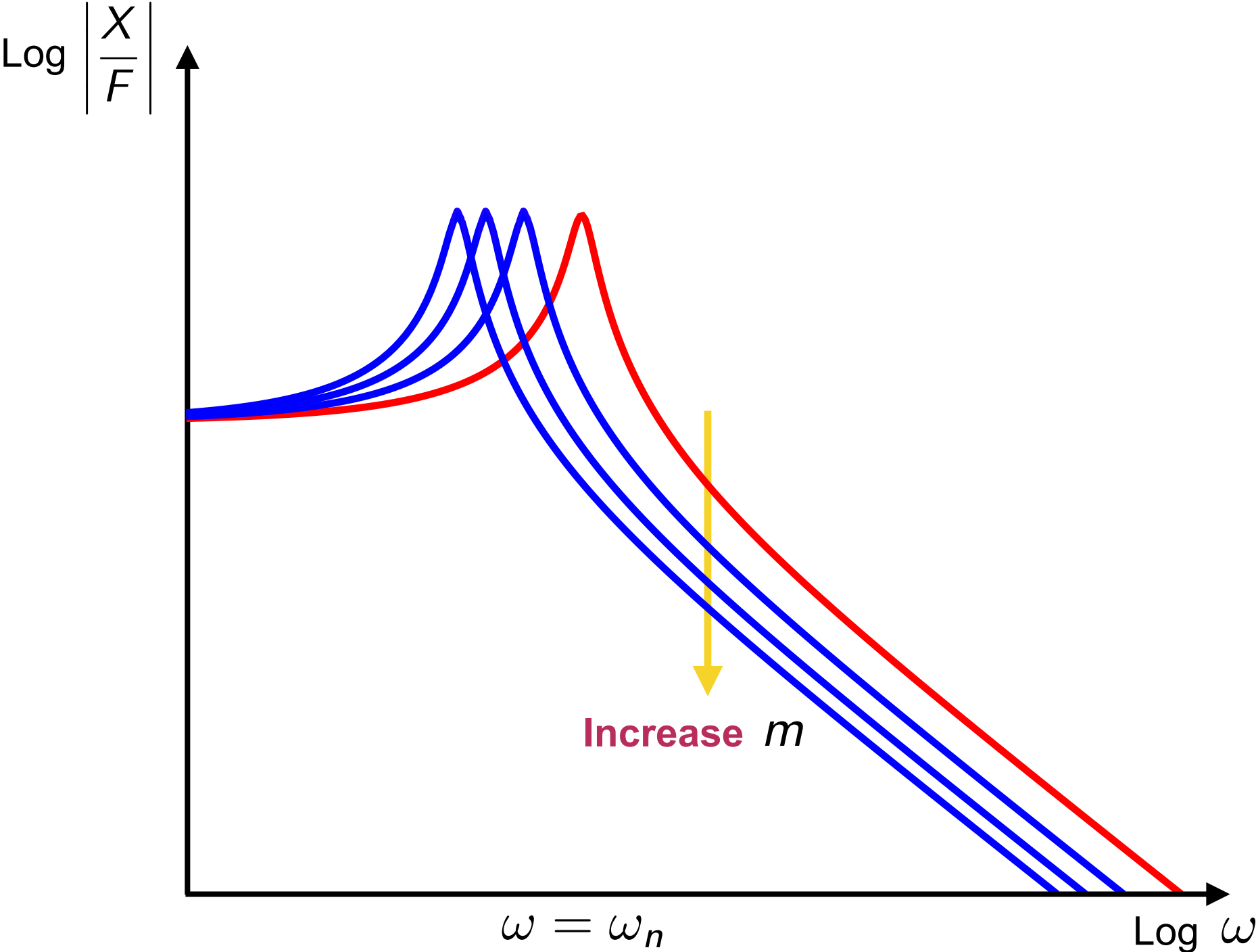
Stiffness controlled



Damping controlled



Mass controlled



How to know the **phase** between the **force** and the **response**?

From (*)

$$\angle \left| \frac{X}{F} \right| = \phi = -\tan^{-1} \left[\frac{\frac{2\zeta\omega}{\omega_n}}{1 - \left(\frac{\omega}{\omega_n} \right)^2} \right]$$

For small ζ :

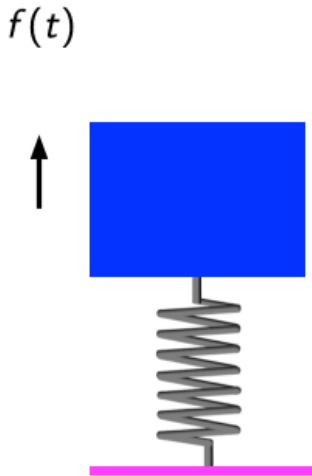
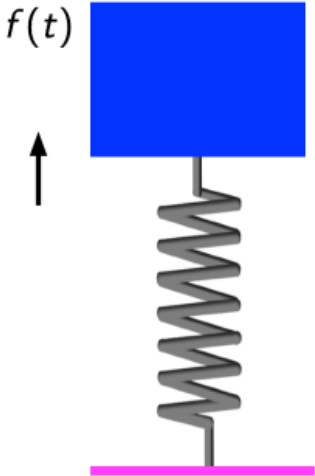
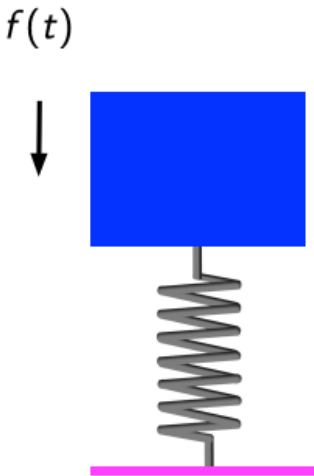
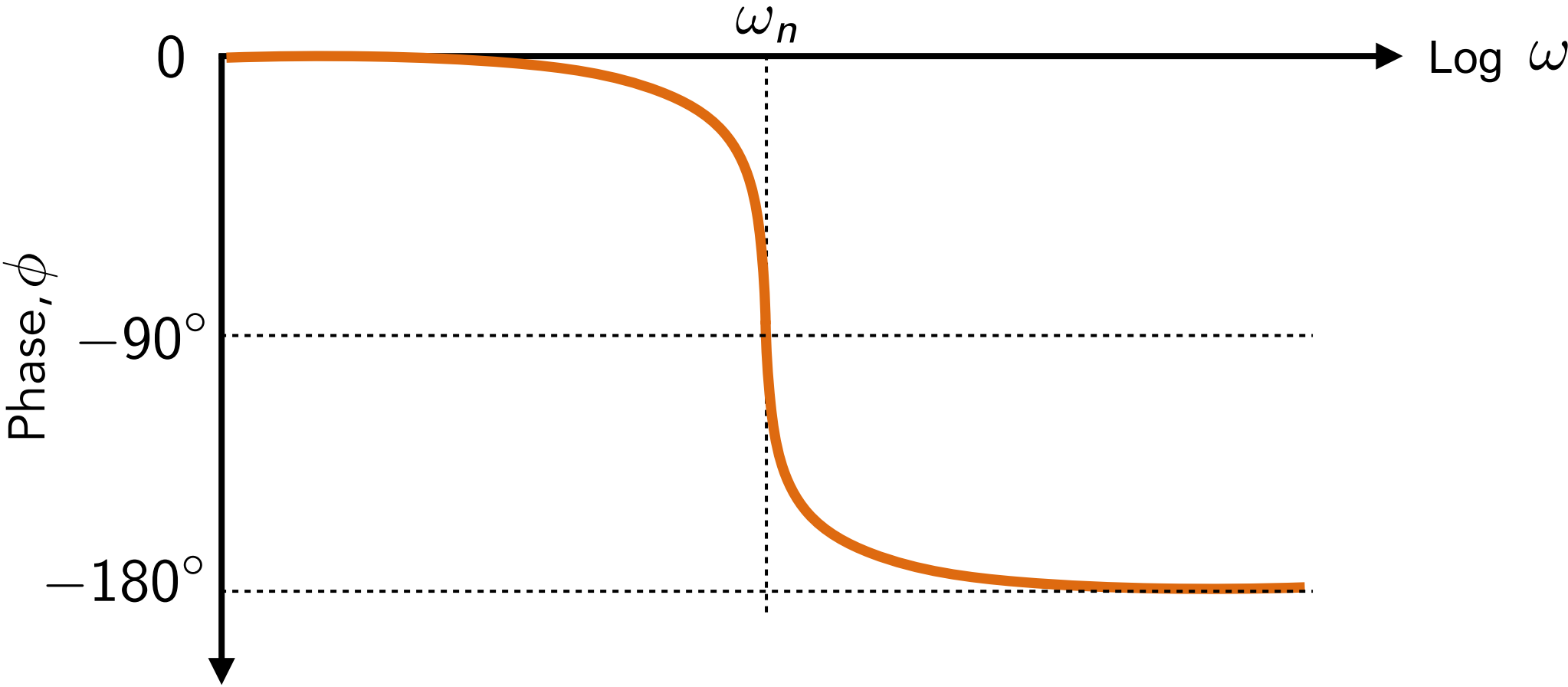
$$\omega \ll \omega_n \Rightarrow \phi \approx -\tan^{-1}(0) = 0$$

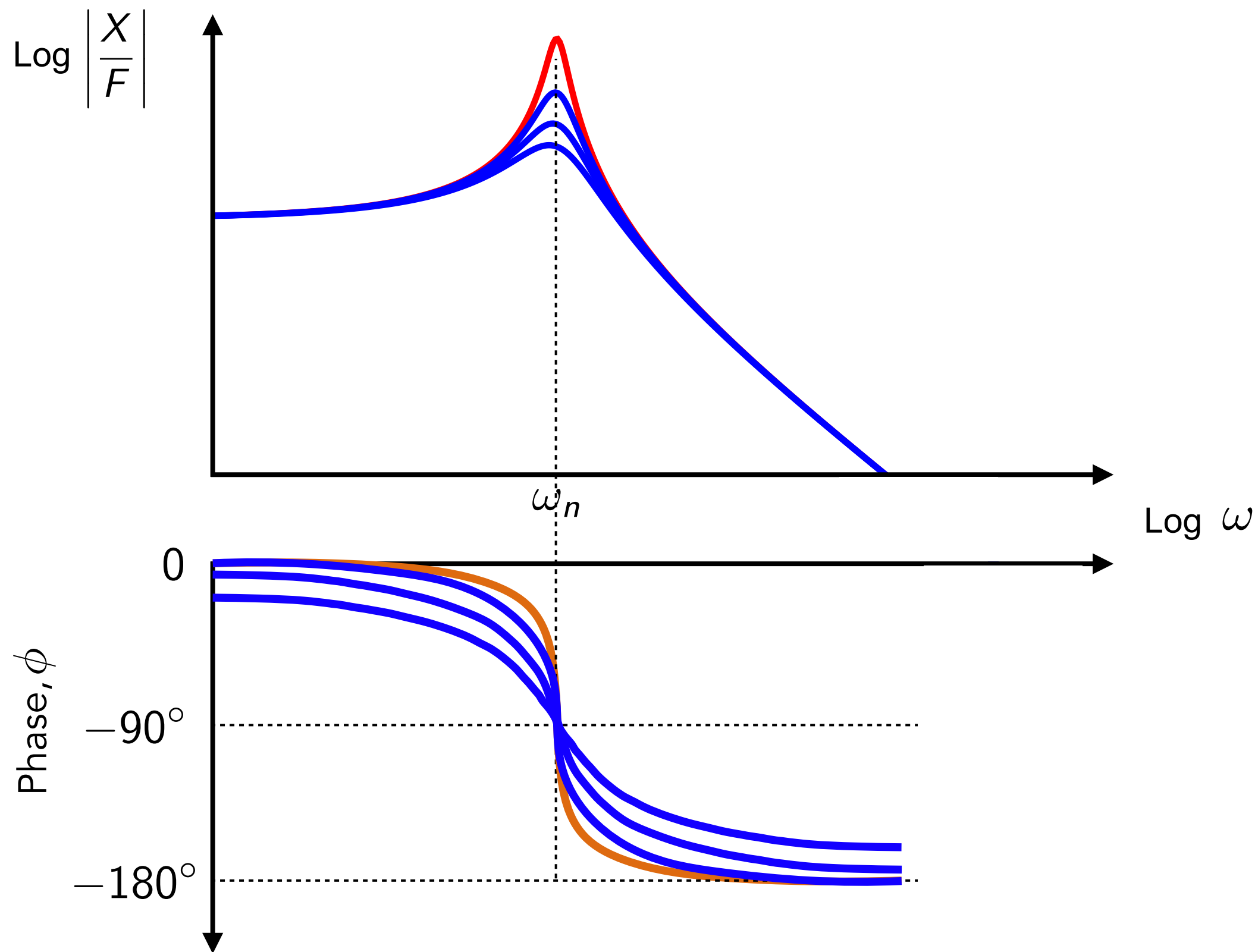
$$\omega = \omega_n \Rightarrow \phi \approx -\tan^{-1}(\infty) = -90^\circ$$

$$\omega \gg \omega_n \Rightarrow \phi \approx \tan^{-1}(0) = -180^\circ$$

Note: If $z = 1/(a + jb)$, the phase is $\phi = -\tan^{-1}(b/a)$

Phase graph

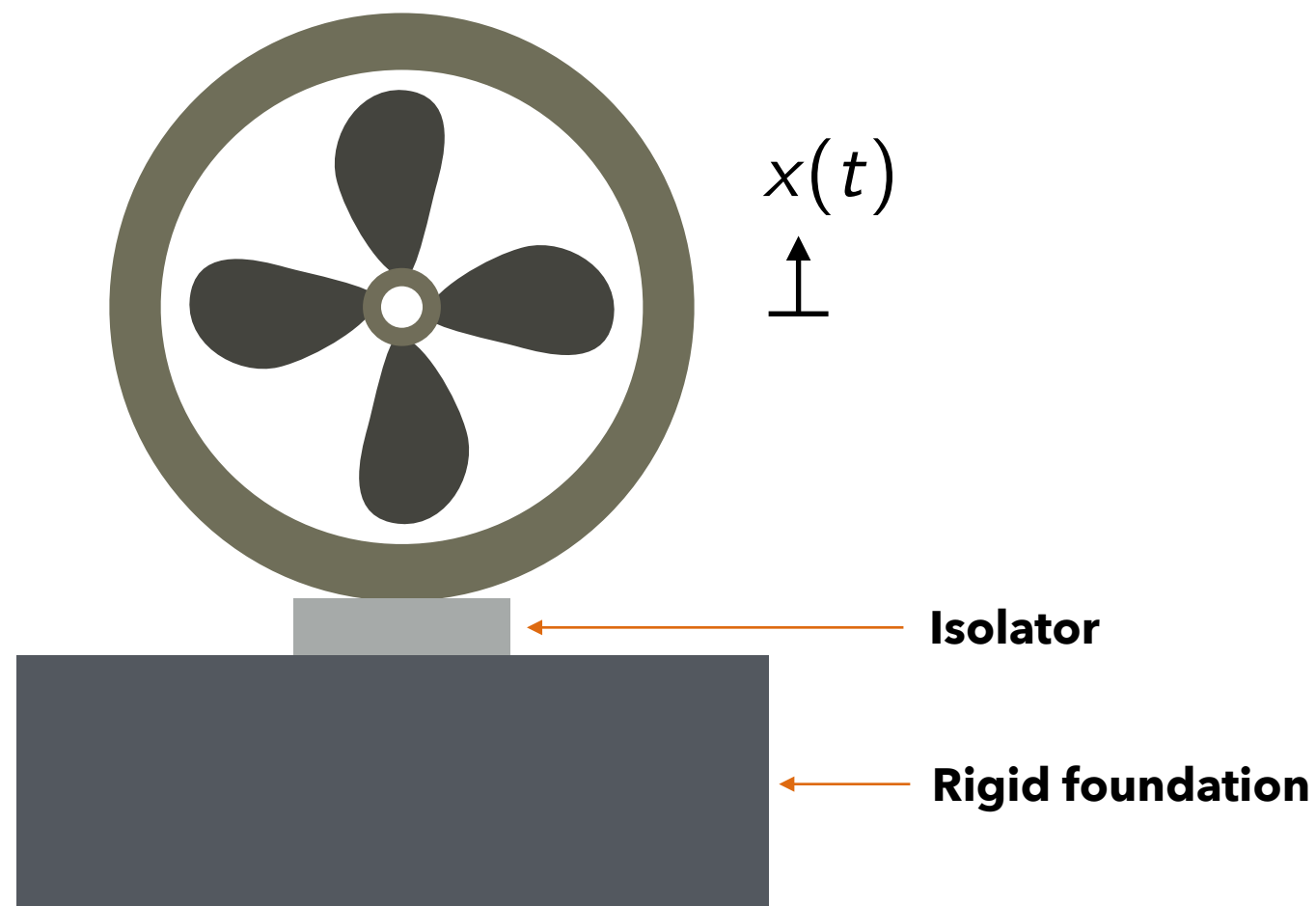




Example 4.2

A 50 kg rotating machine is known to have vertical r.m.s velocity of 8 mm/s. The machine runs at operating frequency of 800 RPM. The machine is rested on rubber isolator with total stiffness constant of 10,000 N/m.

How to effectively reduce the vibration of the machine?



The operating frequency of the machine:

$$f = \frac{900}{60} = 15 \text{ Hz}$$

$$\omega = 2\pi f = 2\pi(15) = 94.2 \text{ rad/s}$$

The natural frequency:

$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{10,000}{50}} = 14.14 \text{ rad/s}$$

The condition: $\omega \gg \omega_n$ (Mass controlled)

Thus the vibration can be effectively reduced by increasing the mass of the machine.

Interact with my animations:

<http://www.azmaputra.com/animations/>



My white-board animation videos:

<http://www.youtube.com/c/AzmaPutra-channel>



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